

AD-A106 320

SCHNABEL ENGINEERING ASSOCIATES RICHMOND VA  
NATIONAL DAM SAFETY PROGRAM, SPRING LAKE DAM (INVENTORY NUMBER --ETC(U)  
MAY 81 R E MARTIN, C S ANDERSON, J G STARR DACW65-81-D-0020

F/G 13/13

UNCLASSIFIED

DACW65-81-D-0020

NL

100  
AD-A106 320

END  
DATE  
FILMED  
11 81  
DTIC

Name Of Dam:

POTOMAC RIVER BASIN

Location:

SPRING LAKE DAM

Inventory Number:

WARREN COUNTY, VIRGINIA

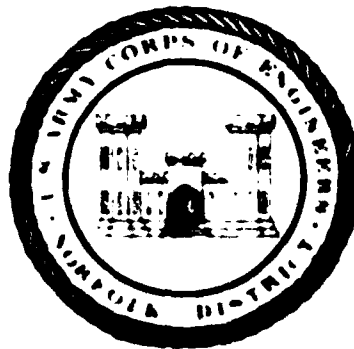
VA. NO. 18703

**LEVEL**

(1)

# PHASE I INSPECTION REPORT

## NATIONAL DAM SAFETY PROGRAM



DTIC  
ELECTE  
OCT 28 1981  
H

PREPARED FOR

NORFOLK DISTRICT CORPS OF ENGINEERS  
803 FRONT STREET  
NORFOLK VIRGINIA 23510

BY

STEVEN H. HARRIS, AREA LIAISON  
1. TOWNSHIP OF AREA LIAISON

01 10 27 218

AD A100320

CFV

ENC 1

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM	
1. REPORT NUMBER VA 18703	2. GOVT ACCESSION NO. AD A106 320	3. RECIPIENT'S CATALOG NUMBER	
4. TITLE (and Subtitle) Phase I Inspection Report National Dam Safety Program Spring Lake Dam Warren County, VA		5. TYPE OF REPORT & PERIOD COVERED Final	
		6. PERFORMING ORG. REPORT NUMBER	
7. AUTHOR(s) Schnabel Engineering Associates, P. C. J. K. Timmons and Associates, Inc.		8. CONTRACT OR GRANT NUMBER(s) DACW-65-81-D-0020	
9. PERFORMING ORGANIZATION NAME AND ADDRESS Schnabel Engineering Associates, P. C. J. K. Timmons and Associates, Inc.		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS	
11. CONTROLLING OFFICE NAME AND ADDRESS U. S. Army Engineer District, Norfolk 803 Front St., Norfolk, VA 23510		12. REPORT DATE May 1981	
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) National Dam Safety Program, Spring Lake Dam (VA Number 18703), Potomac River Basin, Warren County, Virginia. Phase I Inspection Report. (Inventory Number VA 18703) Approved for public release; distribution unlimited		13. NUMBER OF PAGES	
		15. SECURITY CLASS. (of this report) Unclassified	
16. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		15a. DECLASSIFICATION DOWNGRADING SCHEDULE	

## 20. Abstract

Pursuant to Public Law 92-367, Phase I Inspection Reports are prepared under guidance contained in the recommended guidelines for safety inspection of dams, published by the Office of Chief of Engineers, Washington, D. C. 20314. The purpose of a Phase I Inspection is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general conditions of the dam is based upon available data and visual inspection. Detailed investigation and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

Based upon the field conditions at the time of the field inspection and all available engineering data, the Phase I report addresses the hydraulic, hydrologic, geologic, geotechnic, and structural aspects of the dam. The engineering techniques employed give a reasonably accurate assessment of the conditions of the dam. It should be realized that certain engineering aspects cannot be fully analyzed during a Phase I inspection. Assessment and remedial measures in the report include the requirements of additional indepth study when necessary.

Phase I reports include project information of the dam appurtenances, all existing engineering data, operational procedures, hydraulic/hydrologic data of the watershed, dam stability, visual inspection report and an assessment including required remedial measures.

POTOMAC RIVER BASIN

NAME OF DAM: SPRING LAKE DAM  
LOCATION: WARREN COUNTY, VIRGINIA  
INVENTORY NUMBER: VA. NO. 18703

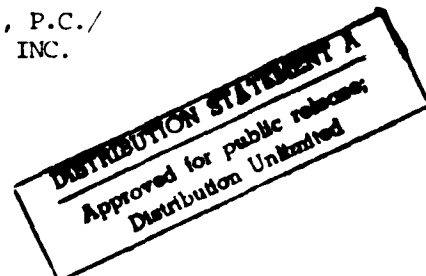
PHASE I INSPECTION REPORT  
NATIONAL DAM SAFETY PROGRAM



PREPARED FOR  
NORFOLK DISTRICT CORPS OF ENGINEERS  
803 FRONT STREET  
NORFOLK, VIRGINIA 23510

BY

SCHNABEL ENGINEERING ASSOCIATES, P.C./  
J. K. TIMMONS AND ASSOCIATES, INC.



# TABLE OF CONTENTS

	Page
Preface . . . . .	i
Brief Assessment of Dam . . . . .	1
Overview Photos . . . . .	4
Section 1: PROJECT INFORMATION . . . . .	5
Section 2: ENGINEERING DATA . . . . .	9
Section 3: VISUAL INSPECTION . . . . .	10
Section 4: OPERATIONAL PROCEDURES . . . . .	13
Section 5: HYDRAULIC/HYDROLOGIC DATA . . . . .	14
Section 6: DAM STABILITY . . . . .	17
Section 7: ASSESSMENT/REMEDIAL MEASURES . . . . .	21

## Appendices:

- I - Maps and Drawings
- II - Photographs
- III - Field Observations
- IV - References

Accession For	
NTIS GRA&I	<input checked="" type="checkbox"/>
DTIC TAB	<input type="checkbox"/>
Unannounced	<input type="checkbox"/>
Justification	
By	
Distribution/	
Availability Codes	
Avail and/or	
Dist Spec Ind	
A	

## PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D. C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

PHASE I REPORT  
NATIONAL DAM SAFETY PROGRAM

BRIEF ASSESSMENT OF DAM

Name of Dam: Spring Lake Dam  
State: Virginia  
Location: Warren County  
USGS Quad Sheet: Linden  
Coordinates: Lat 38° 59.1' Long 78° 02.1'  
Stream: Tributary of Venus Branch  
Date of Inspection: May 5, 1981

Spring Lake Dam is a homogeneous earthfill structure about 300 ft long and 45 ft high. The principal spillway consists of a 15 inch diameter corrugated metal pipe (CMP) riser and a 12 inch diameter CMP outlet which extends through the structure. An earth emergency spillway is located at the right abutment with an 80 ft wide bottom and 3H:1V to 5H:1V side slopes. The dam is classified intermediate in size and is assigned a high hazard classification. The dam is located on a tributary of Venus Branch 2.5 miles east of Shenandoah Farms, Virginia. The lake is used for recreational purposes and is owned and maintained by The Shenandoah Property Owners Association.

Based on criteria established by the Department of the Army, Office of the Chief of Engineers (OCE), the appropriate Spillway Design Flood (SDF) is the PMF. The spillway will pass 60 percent of the Probable Maximum Flood (PMF) or 60 percent of the SDF without overtopping the dam. During the SDF, the dam will be overtopped by a maximum of 0.6 ft for a period of 1 hour and reach a maximum velocity of 3.4 fps. Flows overtopping the dam during the SDF are not considered detrimental to the embankment with respect to erosion. The spillway is judged inadequate, but not seriously inadequate.



The visual inspection revealed no apparent problems. An evaluation of the stability condition could not be made since there is insufficient design and construction data for this structure. The embankment slopes meet U. S. Bureau of Reclamation requirements; however, the embankment crest is narrower than recommended. Based on the visual inspection, the design data and the performance history of the structure, the narrow crest is not considered a serious problem and a stability check is not required.

It is recommended that the owner implement an emergency action plan to warn the downstream dwellings of any dangers which may be imminent.

The following routine maintenance and observation functions should be initiated within the next twelve months:


The grass and weeds on the dam embankment and in the emergency spillways should be cut at least once a year and preferably twice a year. Maintenance is recommended in the early summer and fall. Existing trees on the dam should be cut to the ground. Trees greater than 3 inches in diameter should have their stumps and root structures removed and resulting holes backfilled. The fallen tree(s) adjacent to the principal spillway discharge outlet should be removed.

Vehicular traffic should be restricted on the dam and bare areas on the embankment crest should be reseeded. The toe drain outlet(s) should be located, uncovered and allowed to flow freely. The two iron stained wet areas located to the left of and below the principal spillway discharge outlet should be monitored quarterly to detect any flow which could cause

pipng in the embankment. If increased flows should occur, a geotechnical engineering consultant should be engaged to evaluate the problem. Riprap should be placed below the principal spillway discharge outlet to restrict erosion during flooding. A staff gage should be installed to monitor water levels.

Prepared by:

SCHNABEL ENGINEERING ASSOCIATES, P.C./  
J. K. TIMMONS & ASSOCIATES, INC.

  
Ray E. Martin, Ph.D., P.E.  
Commonwealth of Virginia

Submitted by:

Approved:

Original signed by:  
Carl S. Anderson, Jr.


Carl S. Anderson, Jr., P.E.  
Acting Chief, Design Branch

Original signed by:  
Ronald E. Hudson

Ronald E. Hudson  
Colonel, Corps of Engineers  
Commander and District Engineer

Recommended by:

Original signed by  
JAMES A. WALSH

  
Jack G. Starr  
Chief, Engineering Division

Date:

SEP 11 1981



Spring Lake



Dam

Overview Photographs

1. The first group of people who are likely to be affected by the proposed changes are those who are currently employed in the public sector. This group includes a wide range of individuals, from those in the civil service to those in the health service. The proposed changes are likely to have a significant impact on these individuals, as they will be required to adapt to new ways of working and to new levels of accountability.

• • • •

1. *Environ Biol Fish* (2015) 98:1111–1121. doi:10.1007/s10641-015-0300-1

[illegible]

22

[illegible]

• *Journal of the American Medical Association*, 2000; 284: 2669-2674

The principal spillway consists of a 15 inch diameter corrugated metal pipe (CMP) riser inlet. The riser is connected to a 12 inch diameter CMP outlet which runs through the dam. The riser crest is at elevation 850 msl. An 8 inch diameter sluice gate in the riser at an invert elevation of 818 msl is used to drain the lake. The outlet pipe has a length of 142 ft with an invert elevation at the outlet structure of 810 msl. (See Plate 2, Appendix I).

The emergency spillway (EMS) consists of a vegetated earthen channel located at the right abutment, with a crest elevation of 852.5 msl. The EMS has a bottom width of 80 ft, 3H:1V to 5H:1V side slopes and a cut section (See Plate 3, Appendix I and Field Sketch 1, Appendix II).

1.2.2 Location: Spring Lake Dam is located on a tributary of Venus Branch 2.5 miles east of Shenandoah Farms, Virginia. (See Plate 1, Appendix I)

1.2.3 Size Classification: The dam is classified as an intermediate size structure based on its height as defined in Reference 1, Appendix I.

1.2.4 Hazard Classification: The dam is located in a rural area; however, based upon the proximity of two inhabited dwellings located 1/4 mile downstream, the dam is assigned a "high" hazard classification. The hazard classification used to categorize a dam is a function of location only and has nothing to do with its stability or probability of failure.

1.2.5 Ownership: The dam is owned and maintained by the Shenandoah Farms Property Owners Association.

1. Purpose: Restriction

2. Scope and Instructions: Restriction

3. Objectives: Restriction

4. Methods: Restriction

5. Results: Restriction

6.

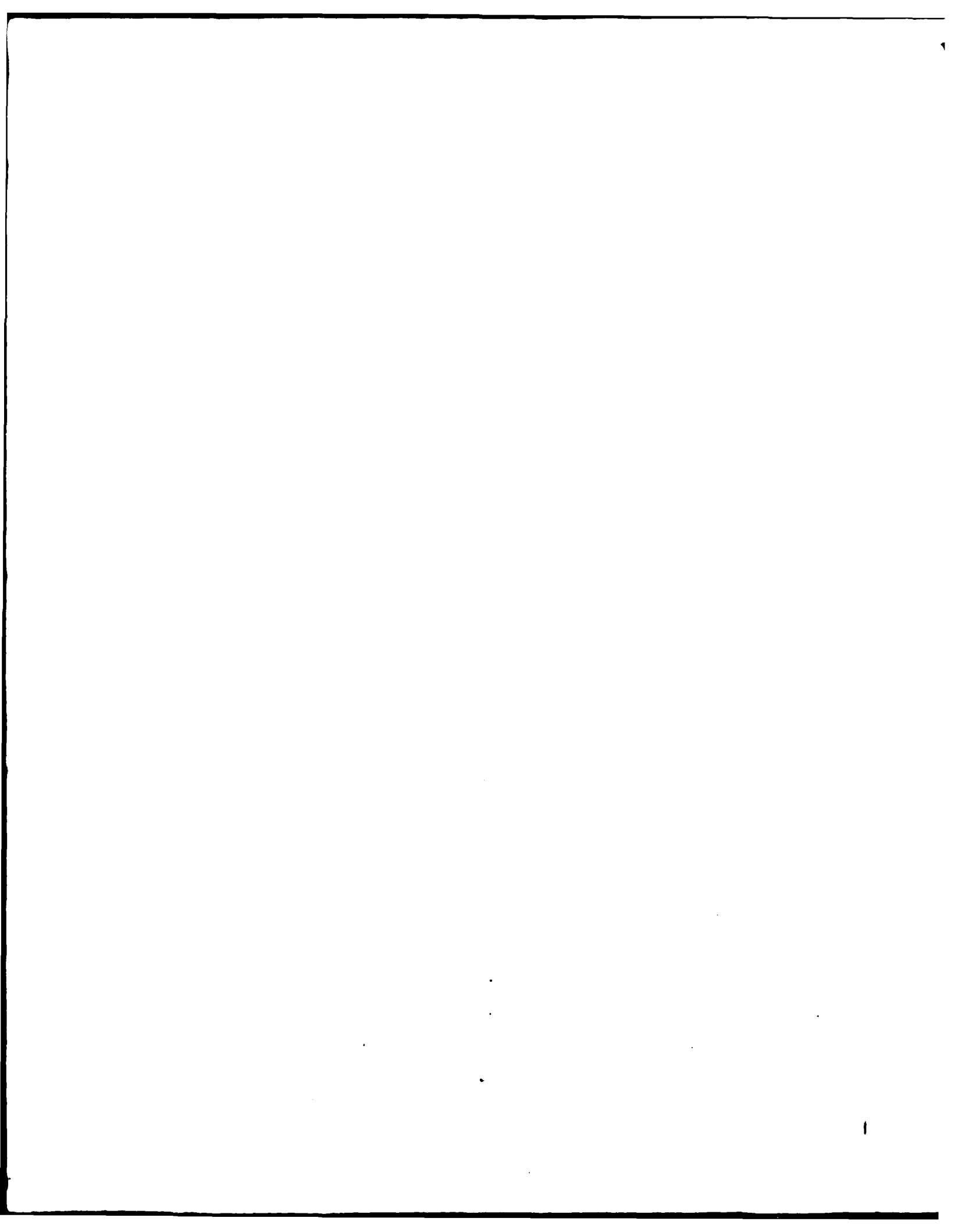
7.

8.









1. The first part of the report is a general  
introduction to the subject of the study.  
2. The second part is a description of the  
methodology used in the study.

3. The third part is a description of the  
results of the study.

4. The fourth part is a discussion of the  
results of the study.

5. The fifth part is a conclusion of the  
study.



#### SECTION 4 - QUALITY PROTECTION

4.1. **Procedure.** The purpose of this section is to ensure that the quality of the highway is maintained. The contractor shall be responsible for the purpose of water infiltration tests on the top of the pavement structure. The water infiltration test shall be performed in accordance with the requirements of the contract. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test.

4.2. **Water Infiltration Test.** The water infiltration test shall be performed in accordance with the requirements of the contract. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test.

4.3. **Water Infiltration Test Results.** The water infiltration test results shall be reported to the Engineer. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test.

4.4. **Water Infiltration Test Results.** The water infiltration test results shall be reported to the Engineer. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test.

4.5. **Water Infiltration Test Results.** The water infiltration test results shall be reported to the Engineer. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test.

4.6. **Water Infiltration Test Results.** The water infiltration test results shall be reported to the Engineer. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test.

4.7. **Water Infiltration Test Results.** The water infiltration test results shall be reported to the Engineer. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test.

4.8. **Water Infiltration Test Results.** The water infiltration test results shall be reported to the Engineer. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test.

4.9. **Water Infiltration Test Results.** The water infiltration test results shall be reported to the Engineer. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test. The contractor shall be responsible for the results of the test.

## SECTION 5. HYDRAULICS/HYDROLOGIC DATA

**Design:** Spring Lake Dam was designed by the Soil Conservation Service and is a single-purpose dam. Hydrologic and hydraulic analyses were conducted.

**Historic Flood Records:** There are no records available.

**Flood Experience:** Information on flooding experience could not be obtained.

**Flood Estimation:** In accordance with the established guidelines, the proposed design flood is based on the estimated "Probable Maximum Flood" for the region of flood discharges that may be expected to occur. A conservative estimation of critical meteorologic and hydrologic conditions that are reasonably possible in the region, or fractions thereof, for the Probable Maximum Flood (PMF) and 5 PMF hydrographs were developed using the HEC-3 method (Reference 4, Appendix IV). Precipitation used for the flood hydrograph of the PMF were taken from U. S. weather bureau information (Reference 5, Appendix IV). Appropriate adjustments for basin size and shape were accounted for. These hydrographs were routed through the reservoir to determine maximum pool elevations.

**Reservoir Regulations:** For routing purposes, the pool at the beginning of flood assumed to be at elevation 850 msl. Reservoir

stage-storage data and stage-discharge data were computed from design details, field sketches and available topographic data.

Floods were routed through the reservoir using the principal spillway discharge up to a pool storage elevation of 852.5 msl and a combined principal and emergency discharges for pool elevations above 852.5 msl. Pool elevations above 855 msl were routed over the non-overflow section of the dam.

5.6 Overtopping Potential: The predicted rise of the reservoir pool and other pertinent data were determined by routing the flood hydrographs through the reservoir as previously described. The results for the flood conditions (PMF and  $\frac{1}{2}$  PMF) are shown in the following

Table 5.1:

Table 5.1 - RESERVOIR PERFORMANCE

	Hydrograph		
	Normal Flow	$\frac{1}{2}$ PMF	PMF
Peak Flow, CFS			
Inflow	11	711	1421
Outflow	11	711	1376
Maximum Pool Elevation			
Ft, msl	856	854.9	853.6
Non-Overflow Section (Elev 855 msl)			
Depth of Flow	-	-	.6
Duration, Hours	-	-	1
Velocity, fps*	-	-	3.4
Tailwater Elevation			
Ft, msl	810	813.6	814.5

\*Critical velocity

5.7 Reservoir Emptying Potential: An 8 inch diameter gate at elevation 818msl is capable of draining the reservoir through the outlet pipe. Assuming that the lake is at normal pool elevation (850 msl) and there is .1 cfs inflow, it would take approximately 3 days to lower the reservoir to elevation 818 msl. This is equivalent to an approximate drawdown rate of 10 ft/day based on the hydraulic height measured from normal pool to the invert of the drawdown pipe divided by the time to dewater the reservoir.

5.8 Evaluation: The U. S. Army, Corps of Engineers' guidelines indicate the appropriate Spillway Design Flood (SDF) for an intermediate size, high hazard dam is the PMF. The spillway will pass 60 percent of the PMF without overtopping the crest of the dam (60 percent of the SDF). During the SDF, the dam will be overtopped by a maximum of 0.6 ft for a period of 1 hour at a maximum velocity of 3.4 fps.

## SECTION 6 - DAM STABILITY

6.1 Foundation and Abutments: The dam is located in the western portion of the Blue Ridge physiographic province of Virginia. The majority of the dam is underlain by the Weverton Formation of Cambrian age; however, the right end of the dam is underlain by the Antietam Formation of late Precambrian age. The Antietam consists essentially of dark to emerald green metakalsalt, purple phyllite and metaconglomerate. The Weverton includes an upper quartz-pebble conglomerate with sandstone interbeds, a middle sandy phyllite with sandstone, and a lower quartz and quartz-pebble conglomerate with interbedded sandy phyllite. The dam is located on an overturned fold which strikes to the northeast and is approximately 60 degrees to the horizontal. The Antietam is exposed to the northeast of the dam and the Weverton to the southwest.

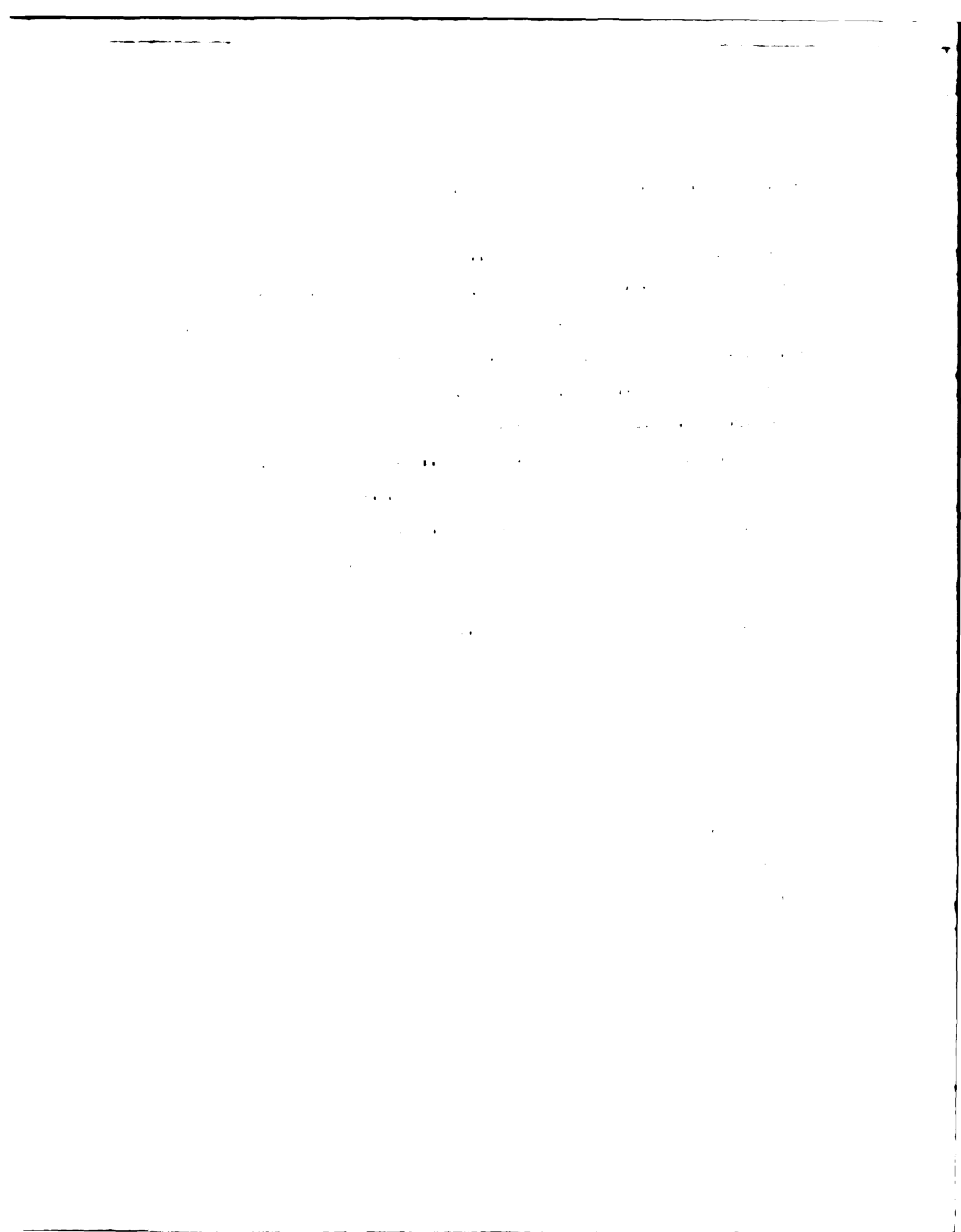
The Antietam is composed of three distinct units. The upper unit is a quartz-pebble conglomerate with sandstone interbeds. The middle unit is a sandy phyllite with sandstone. The lower unit is a quartz and quartz-pebble conglomerate with interbedded sandy phyllite. The dam is located on an overturned fold which strikes to the northeast and is approximately 60 degrees to the horizontal. The Antietam is exposed to the northeast of the dam and the Weverton to the southwest.

The Weverton is composed of three distinct units. The upper unit is a quartz-pebble conglomerate with sandstone interbeds. The middle unit is a sandy phyllite with sandstone. The lower unit is a quartz and quartz-pebble conglomerate with interbedded sandy phyllite. The dam is located on an overturned fold which strikes to the northeast and is approximately 60 degrees to the horizontal. The Antietam is exposed to the northeast of the dam and the Weverton to the southwest.

The Antietam is composed of three distinct units. The upper unit is a quartz-pebble conglomerate with sandstone interbeds. The middle unit is a sandy phyllite with sandstone. The lower unit is a quartz and quartz-pebble conglomerate with interbedded sandy phyllite. The dam is located on an overturned fold which strikes to the northeast and is approximately 60 degrees to the horizontal. The Antietam is exposed to the northeast of the dam and the Weverton to the southwest.



1. The first of these is the fact that the  
the system is not a simple one, but a complex one.  
2. The second is the fact that the system is not a simple one, but a complex one.  
3. The third is the fact that the system is not a simple one, but a complex one.  
4. The fourth is the fact that the system is not a simple one, but a complex one.  
5. The fifth is the fact that the system is not a simple one, but a complex one.  
6. The sixth is the fact that the system is not a simple one, but a complex one.  
7. The seventh is the fact that the system is not a simple one, but a complex one.  
8. The eighth is the fact that the system is not a simple one, but a complex one.  
9. The ninth is the fact that the system is not a simple one, but a complex one.  
10. The tenth is the fact that the system is not a simple one, but a complex one.



Overtopping is not considered a problem because of the small height and duration of flood. Also the velocity of 3.4 fps is less than the effective eroding velocity for a vegetated earth embankment, approximately 6 fps. Some erosion is anticipated on the downstream slope during the toppling; however, it is not considered to be great enough to create a stability problem. Since no undue settlement, cracking, or seepage was noted at the time of inspection, it appears that the embankment is suitable for control storage at elevation 850 msl.

The saturated ground condition present along the downstream toe is believed to be related to flow from the toe drain(s) and also seepage through the dam. Attempts should be made to locate the toe drain outlet(s) and remove any cover material, so as to allow free flow. The two stained areas observed adjacent to and below the discharge pipe are believed to be related to seepage through the dam even though no flow was observed. This does not necessarily create an unsafe condition; however, these areas should be monitored periodically in attempt to detect any significant increases in flow which may result in piping within the embankment.

1000

1000

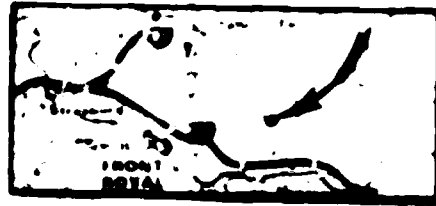
1000

1000

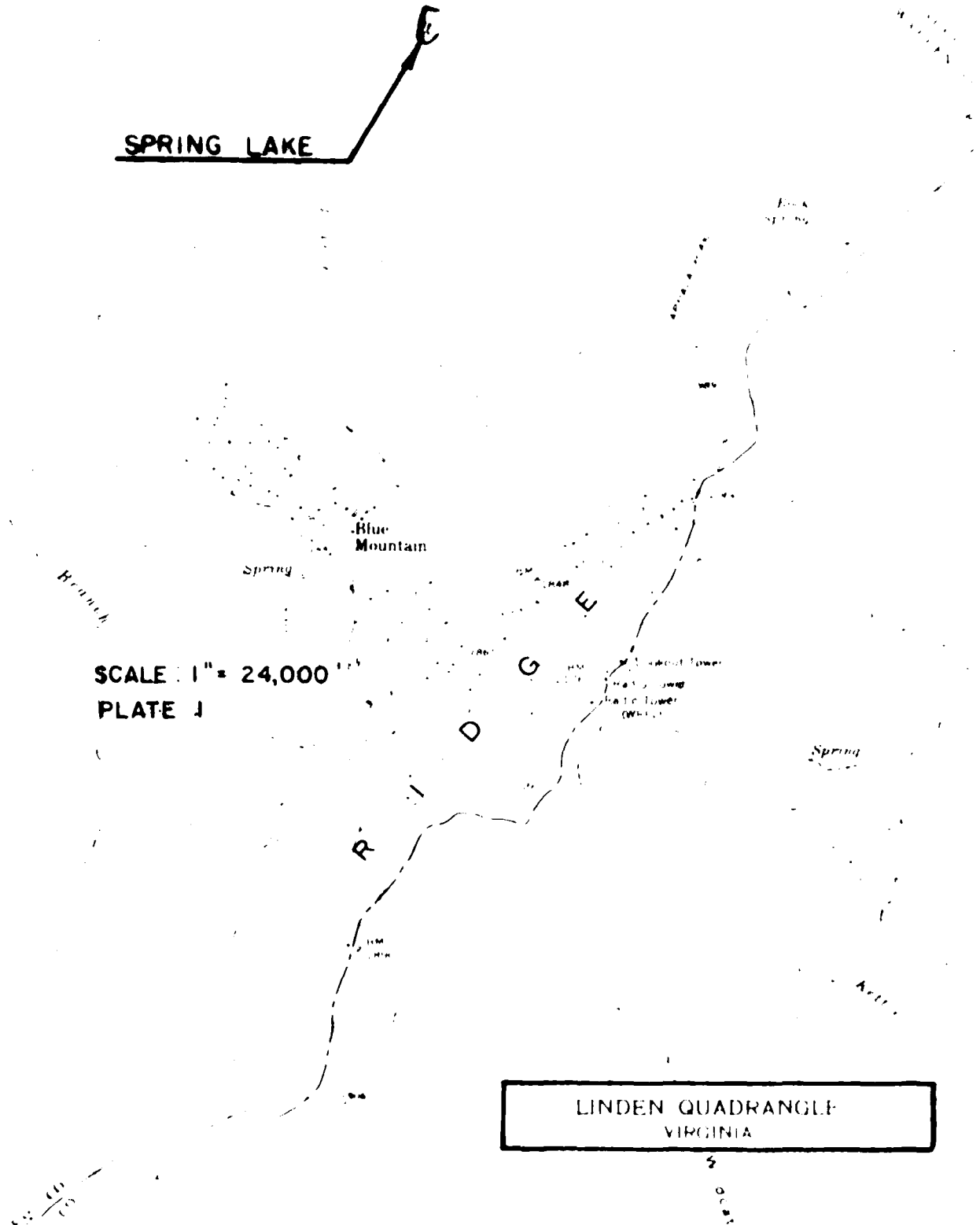
THE UNIVERSITY OF CHICAGO  
DIVISION OF THE PHYSICAL SCIENCES  
DEPARTMENT OF PHYSICS  
530 SOUTH EAST ASIAN AVENUE  
CHICAGO, ILLINOIS 60607-7080  
TEL: 773/936-5000 FAX: 773/936-5001  
WWW: WWW.PHYSICS.UCHICAGO.EDU

1. The first part of the report is a general  
introduction to the subject of the study.  
2. The second part is a description of the  
methodology used in the study.  
3. The third part is a description of the  
results of the study.  
4. The fourth part is a discussion of the  
results of the study.

APPENDIX I  
MAP AND DRAWINGS



SPRING LAKE



LINDEN QUADRANGLE  
VIRGINIA



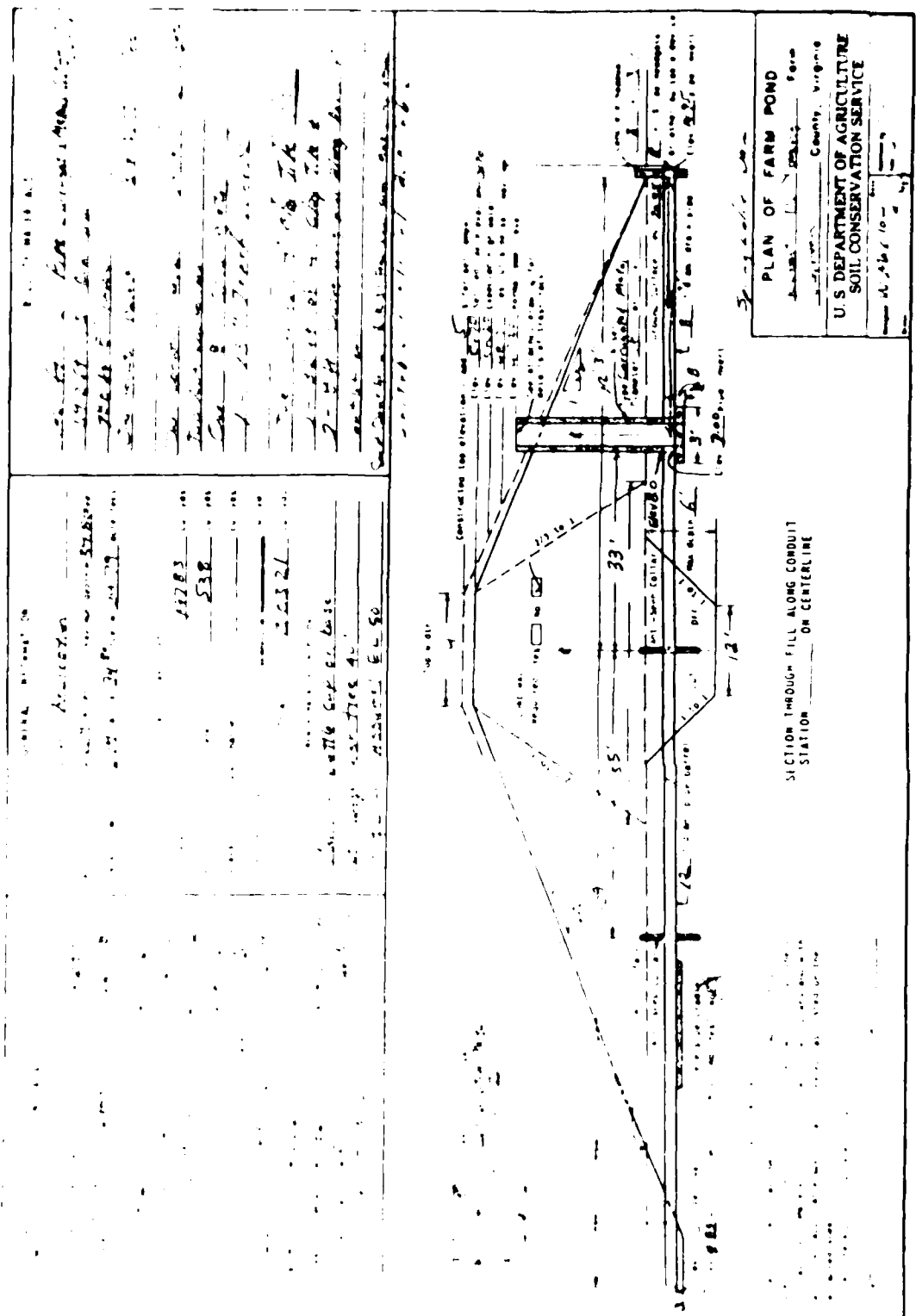


PLATE 2

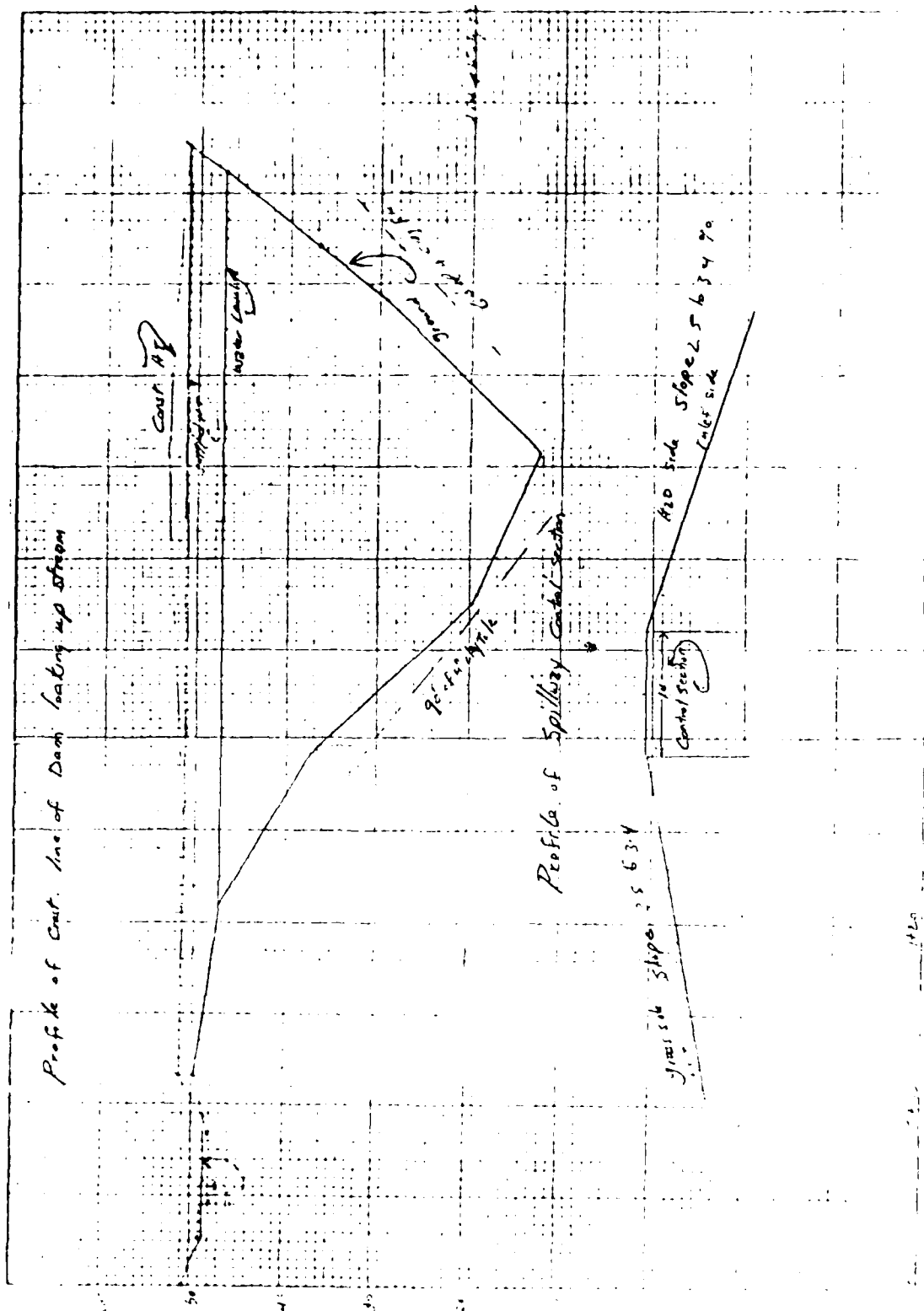


PLATE 3

APPENDIX II

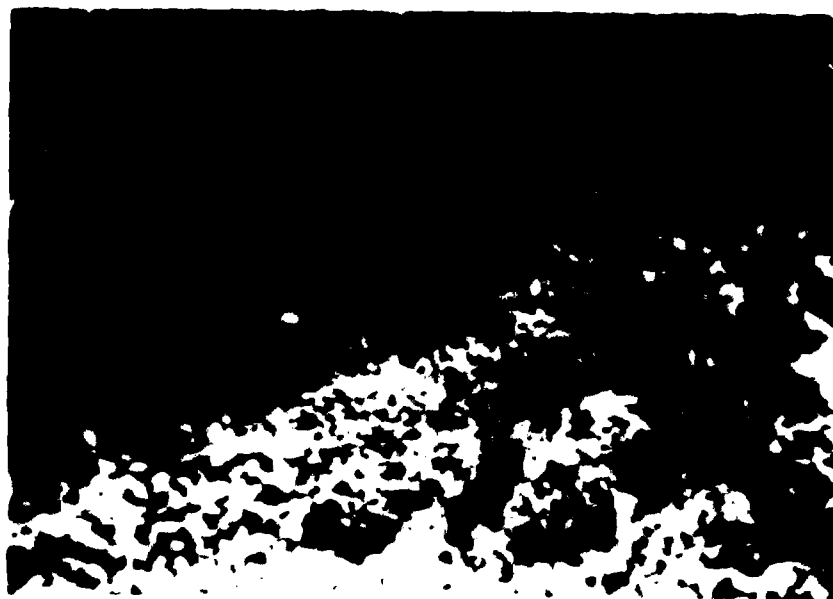
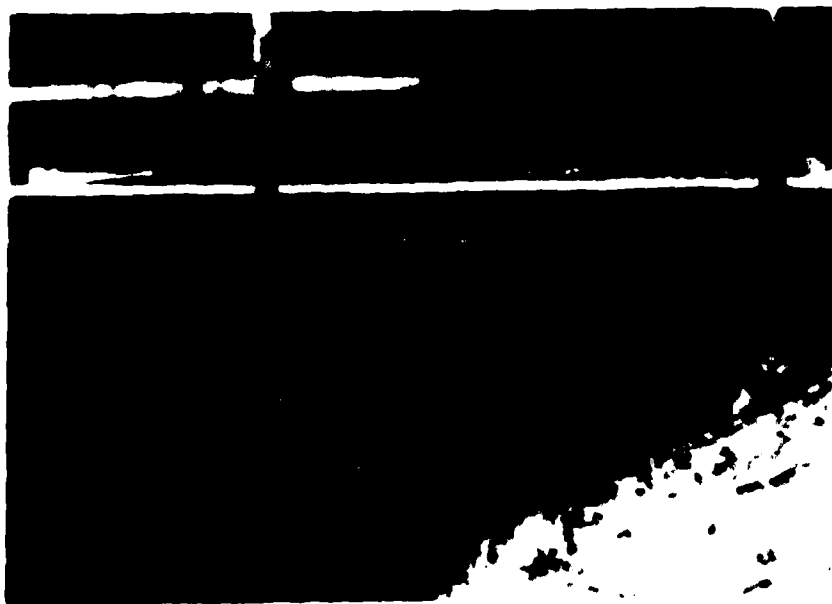
PHOTOGRAPHS

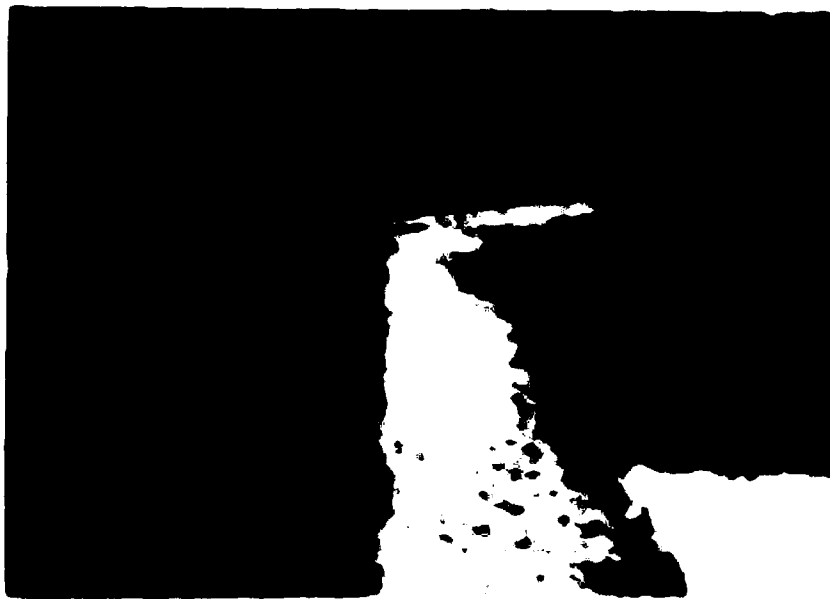


Photograph No. 1 - Upstream Face of Dam



Photograph No. 2 - Downstream Face of Dam





12. 1. 1944  
1. 1. 1944





Vertical and horizontal alignment of the dam

The vertical and horizontal alignment of the dam appeared to be good.

Vertical and horizontal alignment of the dam

The vertical and horizontal alignment of the dam appeared to be good.

Vertical and horizontal alignment of the dam

No riprap was observed.

[illegible][illegible]

THE UNIVERSITY OF CHICAGO

fine to coarse sand, yellowish-brown (SC). Includes

gradient slopes. Crest is  
designed for traffic up to  
100,000 vehicles occur along the  
route. See Field Sketch 1.

---

REMARKS AND RECOMMENDATIONS

---

Principal spillway in good condition.

---

---

Small spillway in good condition.

---





# RESERVOIR

## VISUAL EXAMINATION

## OBSERVATIONS

## REMARKS AND RECOMMENDATIONS

Steep, rocky and heavily wooded slopes bound the left side of the reservoir. Moderate (3H:1V), wooded to open slopes bound the rear and right side. A road bounds the right side. The area appears to be stable. The lake is 2 ft. below the high water mark visible along the upstream slope, above pool level. The reservoir was free of debris.

1/2 acre or more

## SLOPES

Clear water, no apparent sedimentation.

## SEDIMENTATION

DOWNSTREAM CHANNEL

VISUAL EXAMINATION OF

CHANNEL

CONDITION

(CONSTRUCTIONS,  
DEBRIS, ETC.)

Downstream channel is 50 ft wide. Channel is vegetated with grass. Overbanks have an average width of 100 ft.

SLOPES

The slopes are steep to moderate. Slopes are vegetated areas. The flood plain is flat.

APPROXIMATE NO.  
OF HOMES AND  
POPULATION

Two dwellings located on the east side of the channel downstream.

CHECK LIST  
ENGINEERING DATA  
DESIGN, CONSTRUCTION, OPERATION

ITEM	REMARKS
REGIONAL VICINITY MAP	Linden Quadrangle; U.S.G.S. 7 1/2 minute topographic sheet.
DESIGN/CONSTRUCTION HISTORY	The dam was designed by USDA, SCS and constructed by S. W. Vaught. The dam was completed in 1968.
PLAN OF DAM	See Plates 2 and 3, Appendix III.
TYPICAL SECTIONS OF DAM	See Plates 2 and 3, Appendix III.
OUTLETS - PLAN DETAILS CONSTRAINTS DISCHARGE RATINGS	See Plates 2 and 3, Appendix III.
SPILLWAY - PLAN SECTION DETAILS	See Field Sketch.
OPERATING EQUIPMENT - PLAN DETAILS	Not available.



1000000

1000000

1000000

1000000

1000000

1000000

1000000

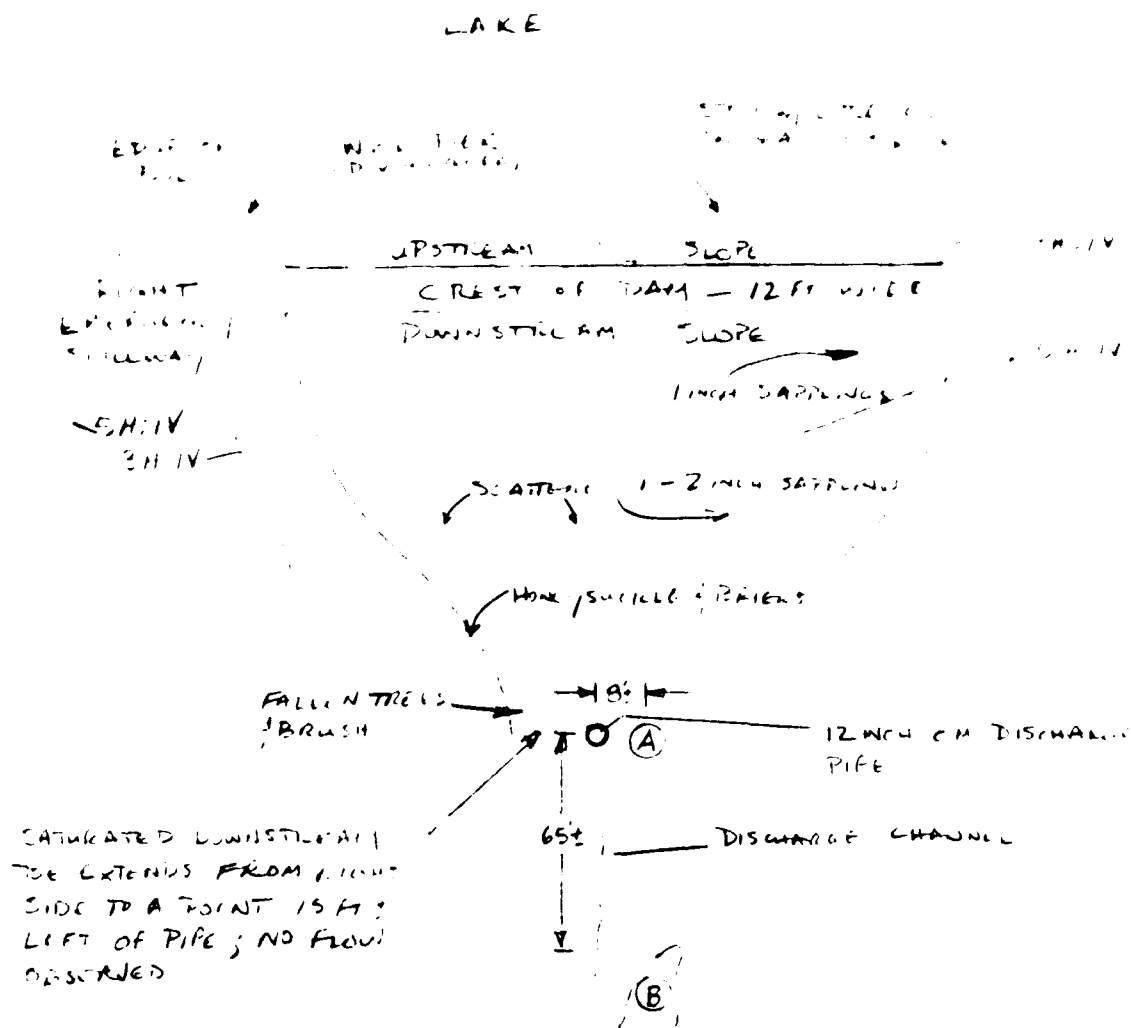
1. IDENTIFICATION  
 2. DESCRIPTION OF FAILURE  
 3. ANALYSIS OF FAILURE  
 4. RECOMMENDATIONS

1. IDENTIFICATION  
 2. DESCRIPTION OF FAILURE  
 3. ANALYSIS OF FAILURE  
 4. RECOMMENDATIONS

1. IDENTIFICATION

1. IDENTIFICATION  
 2. DESCRIPTION OF FAILURE  
 3. ANALYSIS OF FAILURE  
 4. RECOMMENDATIONS

1. IDENTIFICATION



(A) RED IRON STAINED SEC-PAGE; NO FLOW OBSERVED.

(B) RED IRON STAINED PONDED AREA 40 FT ± LONG AND 10 FT ± WIDE; NO FLOW OBSERVED.

NOTE: EMBANKMENT 300 FT ± LONG  
EMS 80 FT ± WIDE

... ..  
... ..  
... ..

... ..  
... ..  
... ..

... ..  
... ..  
... ..

END

DATE  
FILMED

11-81

DTIC